

Small Outlet - maintenance



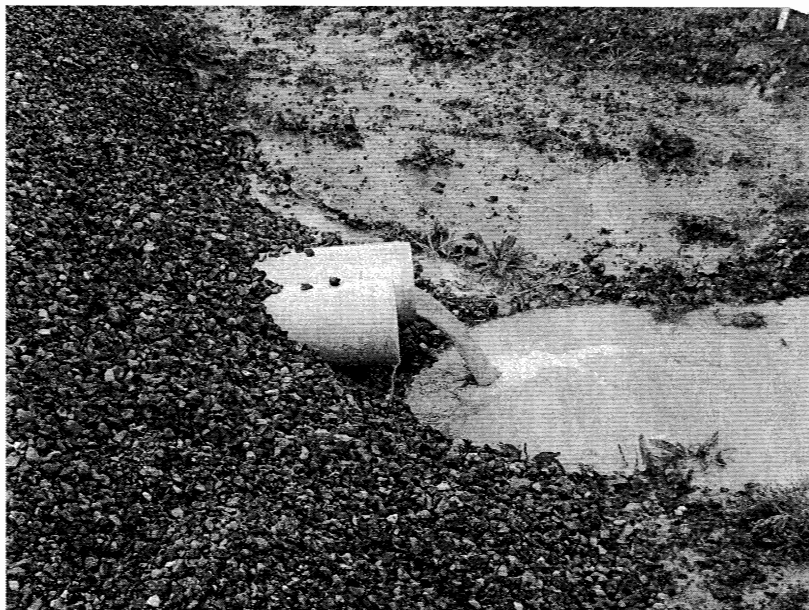
Small Pond - Inlet



Outlet capacity - pipe in inlet control



Outlet capacity - pipe in inlet control



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Outlet capacity - pipe in inlet control



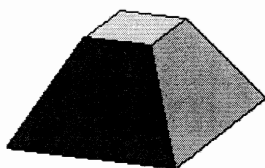
Outlet capacity - pipe in inlet control



Pond Volumes - Frustum

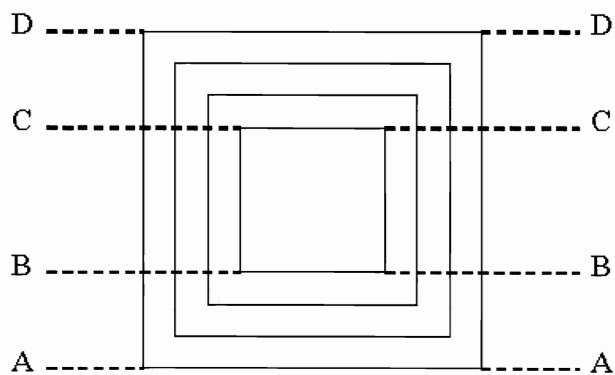
- For a square pond with uniform side slope - three methods:
 - Frustum of a pyramid (exact)
 - Average end area
 - Area of contours
- Volume of frustum of a pyramid
 - $V = h(B_1 + B_2 + [B_1 * B_2]^{0.5}) / 3$
 - For 40' x 40' base, 4' deep pond, with 4:1 side slopes
 - $B_1 = 40 * 40 = 1600 \text{ sq ft}$
 - $B_2 = (40 + 16 + 16) * (40 + 16 + 16) = 5184 \text{ sq ft}$
 - $V = 4(1600 + 5184 + [1600 * 5184]^{0.5}) / 3$
 - $V = 12,885 \text{ cu. ft.}$

Pond Volumes - Average end area



- Average end area (4 cross-sections)
 - Section A-A = 0 sq ft
 - Section B-B = $0.5 * 4 * (40 + 72) = 224$ sq ft
 - Section C-C = Section B-B = 224 sq ft
 - Section D-D = 0 sq ft

Pond Volumes - Average end area



SECTION B-B

Pond Volumes - Average end area

Distance	Area	Volume	Total Volume
0	0		
		1792	1792
16	224		
		8960	10752
56	224		
		1792	12544
72	0		

• V = 12,544 cu. ft. difference of -2.65%

Pond Volumes - 1-foot contours

• Area of contours						
– 1 foot contours:						
Depth	Length	Width	Area	Avg. Area	Incr. Vol	Total Vol
0	40	40	1600			
				1952	1952	1952
1	48	48	2304			
				2720	2720	4672
2	56	56	3136			
				3616	3616	8288
3	64	64	4096			
				4640	4640	12928
4	72	72	5184			

– V = 12,928 cu. ft. difference of +0.33%

Pond Volumes - 2-foot contours

- Area of contours

- 2 foot contours:

Depth	Length	Width	Area	Avg. Area	Incr. Vol	Total Vol
0	40	40	1600			
				2368	4736	4736
2	56	56	3136			
				4160	8320	13056
4	72	72	5184			

– V = 13,056 cu. ft. difference of +1.32%

Pond Volumes - 4-foot contours

- Area of contours

- 4 foot contours:

Depth	Length	Width	Area	Avg. Area	Incr. Vol	Total Vol
0	40	40	1600			
				3392	13568	13568
4	72	72	5184			

– V = 13,568 cu. ft. difference of +5.30%

Pond Volumes - method comparison

- Frustum of a pyramid (exact), $V = 12,885$ cu. ft.
- Average End Area, $V = 12,544$ cu. ft. difference of - 2.65%
- Area of contours
 - 1 foot contours, $V = 12,928$ cu. ft. difference of +0.33%
 - 2 foot contours, $V = 13,056$ cu. ft. difference of +1.32%
 - 4 foot contours, $V = 13,568$ cu. ft. difference of +5.30%

Hydrograph Routing

- Inflow - Outflow = Change in Storage
 $Q_{in} * \Delta t - Q_{out} * \Delta t = \Delta S$
- Required Information:
 - Inflow Hydrograph
 - Outlet Stage-Discharge Curve
 - Pond Stage-Storage Curve
- Example: Using Rational Method Hydrograph developed previously for 10-year, one-hour event for a 10-acre parking lot in Ottumwa, IA, an 18-inch diameter discharge pipe at the bottom of the pond, and a 100' x 100' square pond with 4:1 side slopes, route the hydrograph through the pond

Hydrograph Routing - Inflow

- Inflow Hydrograph

Clock time minutes	Q, cfs
0	0.0
10	8.7
20	24.1
30	56.4
40	18.6
50	8.7
60	8.7

Pond Volumes - Size approximation

- Inflow Hydrograph

Clock time minutes	Q, cfs	Volume cubic feet
0	0.0	0
10	8.7	5,220
20	24.1	14,460
30	56.4	33,840
40	18.6	11,160
50	8.7	5,220
60	8.7	5,220
Total		75,120

- Upper limit: total flow = 75,120 cubic feet
- Lower limit: total flow - maximum discharge
If max. discharge=14 cfs: $75,120 - (14)(60)(60) = 24,720$ cf

Hydrograph Routing - pond volume

- Volume of frustum of a pyramid
 - $V = h(B_1 + B_2 + [B_1 \cdot B_2]^{0.5})/3$
 - For 100' x 100' base, 4' deep pond, with 4:1 side slopes
 - $B_1 = 100 \times 100 = 10,000 \text{ sq ft}$
 - $B_2 = (100 + 16 + 16) \times (100 + 16 + 16) = 17,424 \text{ sq ft}$
 - $V = 4(10000 + 17424 + [10000 \cdot 17424]^{0.5})/3$
 - $V = 54,165 \text{ cu. ft.}$
 - Solving for depth at 0.5 foot increments yields the stage-storage curve for the pond

Hydrograph Routing - Stage-Storage-Discharge

- Stage-Storage-Discharge Curve for 100' x 100' pond, 4 foot deep with 4:1 sides:

Depth	Flow	Storage	Depth	Flow	Storage	Depth	Flow	Storage
0.1	0.1	1008	1.5	5.1	16872	2.9	9.5	36248
0.2	0.1	2032	1.6	5.6	18135	3.0	9.7	37776
0.3	0.2	3073	1.7	6.1	19417	3.1	9.9	39324
0.4	0.5	4129	1.8	6.6	20716	3.2	10.1	40891
0.5	0.7	5203	1.9	7.0	22034	3.3	10.3	42479
0.6	1.0	6293	2.0	7.3	23371	3.4	10.5	44086
0.7	1.3	7399	2.1	7.6	24726	3.5	10.7	45715
0.8	1.7	8523	2.2	7.8	26099	3.6	10.9	47363
0.9	2.1	9664	2.3	8.1	27492	3.7	11.1	49033
1.0	2.6	10821	2.4	8.3	28903	3.8	11.3	50723
1.1	3.0	11996	2.5	8.5	30333	3.9	11.5	52433
1.2	3.5	13189	2.6	8.8	31783	4.0	11.7	54165
1.3	4.1	14399	2.7	9.0	33252			
1.4	4.6	15627	2.8	9.3	34740			

Hydrograph Routing - First time increment

- Time increment 10 minutes:
 - Inflow = 8.7 cfs
 - Inflow = $8.7 * 60 \text{ (sec/min)} * 10 \text{ min} = 5220 \text{ cubic feet}$
 - Trial volume = 5220 cubic feet
 - Trial depth = 0.5 ft
 - Average depth = 0.25 ft
 - Outflow = 0.2 cfs
 - Outflow = $0.2 * 60 * 10 = 120 \text{ cubic feet}$
 - Cumulative Storage = $5220 - 120 = 5100 \text{ cubic feet}$
 - Depth at this volume $\sim 0.5 \text{ ft}$, = Trial depth, continue with next time increment

Hydrograph Routing - Second time increment

- Time increment 20 minutes:
 - Inflow = 24.1 cfs
 - Inflow = $24.1 * 60 * 10 = 14,460 \text{ cubic feet}$
 - Trial volume = $14460 + 5100 = 19,560 \text{ cubic feet}$
 - Trial depth = 1.7 ft
 - Average depth = $(1.7 + 0.5)/2 = 1.1 \text{ ft}$
 - Outflow = 3.0 cfs
 - Outflow = $3.0 * 60 * 10 = 1800 \text{ cubic feet}$
 - Cumulative Storage = $19,560 - 1800 = 17,760 \text{ cubic feet}$
 - Depth at this volume $\sim 1.6 \text{ ft} < \text{Trial depth}$, continue with another iteration

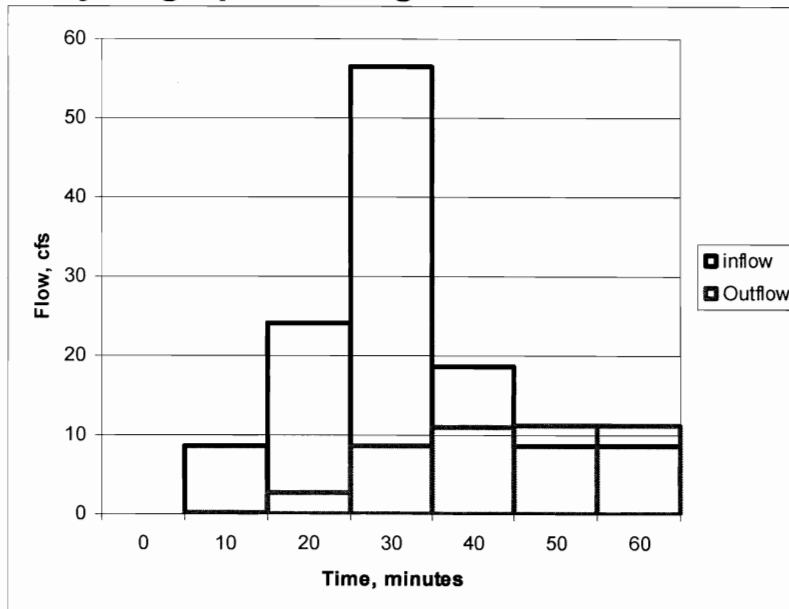
Hydrograph Routing - Second time increment

- Time increment 20 minutes, second iteration:
 - Inflow = 24.1 cfs
 - Inflow = $24.1 * 60 * 10 = 14,460$ cubic feet
 - Trial volume = $14460 + 5100 = 19,560$ cubic feet
 - Trial depth (from first iteration) = 1.6 ft
 - Average depth = $(1.6 + 0.5)/2 = 1.05$ ft
 - Outflow = 2.8 cfs
 - Outflow = $2.8 * 60 * 10 = 1680$ cubic feet
 - Cumulative Storage = $19,560 - 1680 = 17,880$ cubic feet
 - Depth at this volume ~ 1.6 ft = Trial depth, continue with next time increment

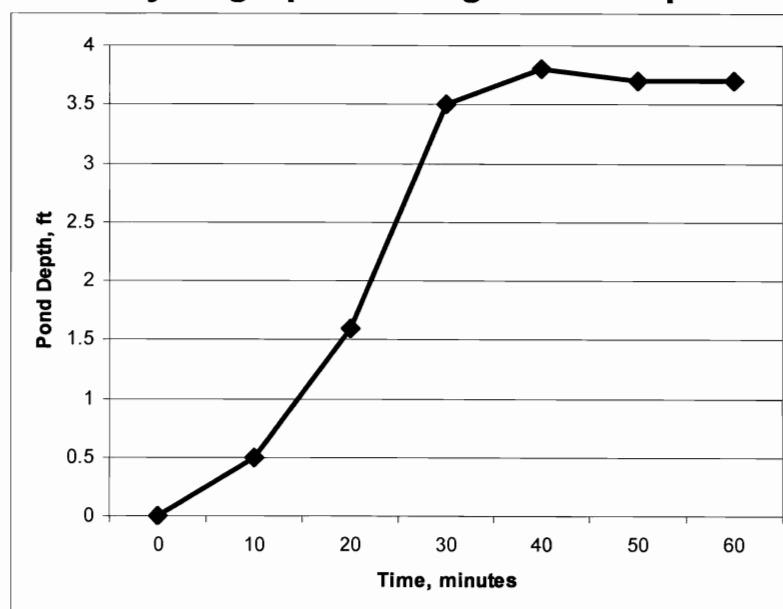
Hydrograph Routing - Table

Time	Inflow cfs	Inflow cu ft	Trial Volume cu ft	Trial Depth ft	Average Depth ft	Outflow cfs	Outflow cu ft	Volume cu ft
0	0	0	0	0	0	0	0	0
10	8.7	5220	5220	0.5	0.25	0.2	120	5100
20	24.1	14460	19560	1.7 1.6	1.1 1.05	3.0 2.8	1800 1680	17760 17880
30	56.4	33840	51720	3.9 3.5	2.75 2.55	9.1 8.6	5460 5160	46260 46560
40	18.6	11160	57720	4.0 3.8	3.75 3.65	11.2 11.0	6720 6600	51000 51120
50	8.7	5220	56340	4.0 3.7	3.9 3.75	11.5 11.2	6900 6720	49440 49620
60	8.7	5220	54840	4.0 3.6 3.7	3.85 3.65 3.7	11.4 11.0 11.1	6840 6600 6660	48000 48240 48180

Hydrograph Routing - Inflow vs. Outflow



Hydrograph Routing - Pond depth



Hydrograph Routing - Class Problem

- Class Problem: Using Rational Method Hydrograph developed previously for 5-year, one-hour event for a 5-acre parking lot in Red Wing, MN, an 18-inch diameter discharge pipe at the bottom of the pond, and a 100' x 100' square pond with 4:1 side slopes, route the hydrograph through the pond

Routing Problem - Inflow

- Inflow Hydrograph, Class Problem

Clock time	Q, cfs
minutes	
0	0.0
10	3.2
20	8.7
30	20.5
40	6.6
50	3.2
60	3.2

Routing Problem - Stage-Storage-Discharge

- Stage-Storage-Discharge Curve for 100' x 100' pond, 4 foot deep with 4:1 sides:

Depth (ft)	Volume (cu.ft.)	Discharge (cfs)
0.0	0	0.0
0.5	5203	0.7
1.0	10821	2.5
1.5	16872	5.1
2.0	23371	7.7
2.5	30333	8.7
3.0	37776	9.8
3.5	45715	10.8
4.0	54165	12.2

Hydrograph Routing - Stage-Storage-Discharge

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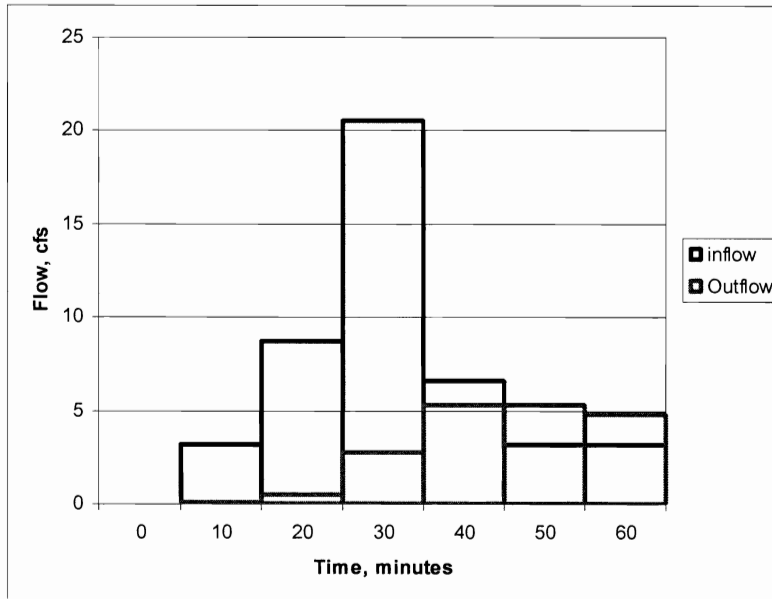
Routing Problem - Table

Time	Inflow cfs	Inflow cu ft	Trial Volume cu ft	Trial Depth ft	Average Depth ft	Outflow cfs	Outflow cu ft	Volume cu ft
0	0	0	0	0	0	0	0	0
10	3.2							
20	8.7							
30	20.5							
40	6.6							
50	3.2							
60	3.2							

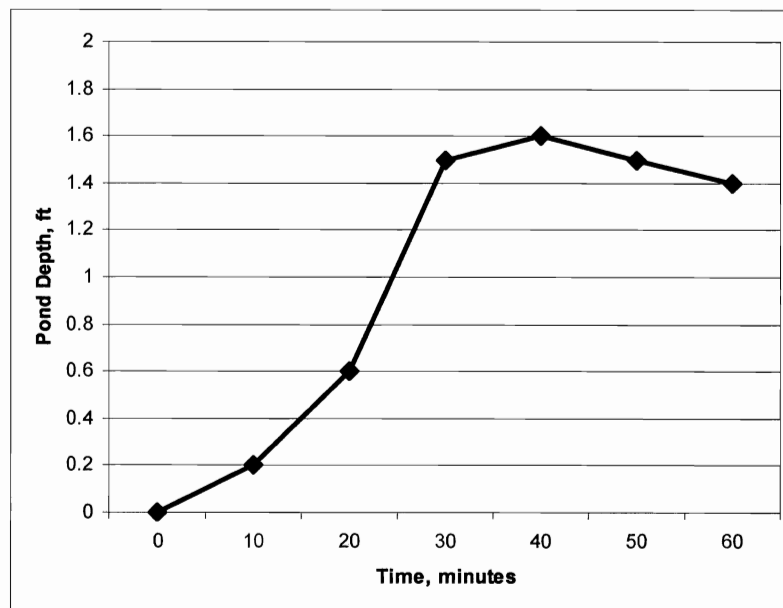
Routing Problem - Table

Time	Inflow cfs	Inflow cu ft	Trial Volume cu ft	Trial Depth ft	Average Depth ft	Outflow cfs	Outflow cu ft	Volume cu ft
0	0	0	0	0	0	0	0	0
10	3.2	1920	1920	0.2	0.1	0.1	60	1860
20	8.7	5220	7080	0.7 0.6	0.45 0.4	0.6 0.5	360 300	6720 6780
30	20.5	12300	19080	1.7 1.5	1.15 1.05	3.2 2.8	1920 1680	17160 17400
40	6.6	3960	21360	1.8 1.6	1.65 1.55	5.8 5.3	3480 3180	17880 18180
50	3.2	1920	20100	1.8 1.5	1.7 1.55	6.1 5.3	3660 3180	16440 16920
60	3.2	1920	18840	1.7 1.4	1.6 1.45	5.6 4.8	3360 2880	15480 15960

Routing Problem - Inflow vs. Outflow



Routing Problem - Pond depth



Pond Geometry

- Generally constrained by site topography or development
- For better treatment, length should be 2 times width or more
- Rectangular may be most efficient and easiest to construct, but not aesthetically pleasing
- Outlet should be as far away from inlet as physically possible
- Side slopes:
 - 2H:1V minimum for stability, but people can't traverse when wet
 - 4H:1V probably minimum for mowing and walking
 - Flatter better for aesthetics, but not efficient use of land area and may create too much shallow water (WNV)

Water Quality Impacts

- Detention for water quality often requires substantial time of detention for "first flush" (often first 0.5 to 1.0 inch of runoff) or frequent return periods (6-months to 2-years)
- Parking lot pollutants include TSS, Cadmium, Copper, Lead, Zinc, Oil and Grease
- Wet Ponds
 - Generally require 12-48 hours of "hydraulic residence time" to achieve significant treatment
 - 90% of pollutant removal occurs during the quiescent period (period between rainfall events)
 - Improper design/location/maintenance can result in adverse effects on water quality, groundwater, cold water fisheries or wetlands

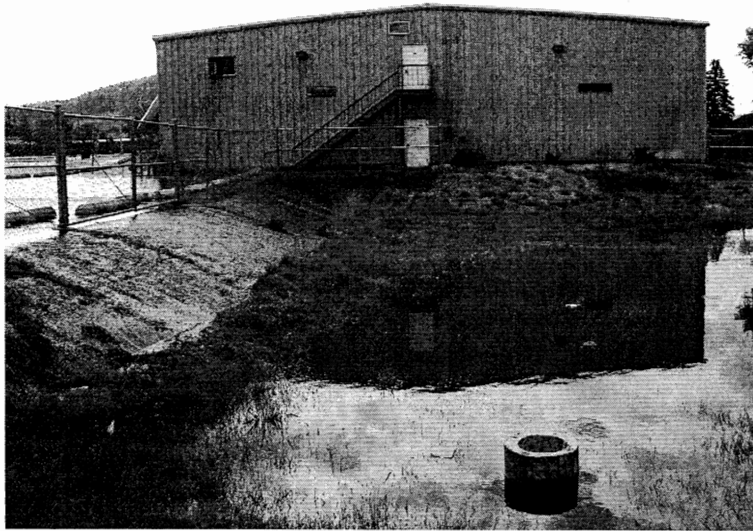
Water Quality - Wet Ponds

- Wet Ponds
 - Rectangular shapes subject to short-circuiting of flow
 - Must be able to maintain a permanent pool of water
 - Insufficient precipitation
 - Permeable soils
 - Small drainage areas
 - Land requirements can be a constraint, especially in developed areas
 - Poor maintenance can substantially reduce performance – Pollutant storage vs. pollutant removal

Water Quality - Dry Ponds

- Dry Detention Ponds
 - Provide very little pollutant removal, primarily due to short HRT
 - Can provide some limited reduction of larger sediments (sands and gravels)
 - Effective for flood control
- Dry Extended Detention Ponds
 - Land requirements can be a constraint, especially in developed areas
 - Maintenance can substantially reduce performance
 - Moderate pollutant removal and ineffective at removing soluble pollutants, though removal rates are highly variable

Pond adjacent to Parking Lot



Potential Pond



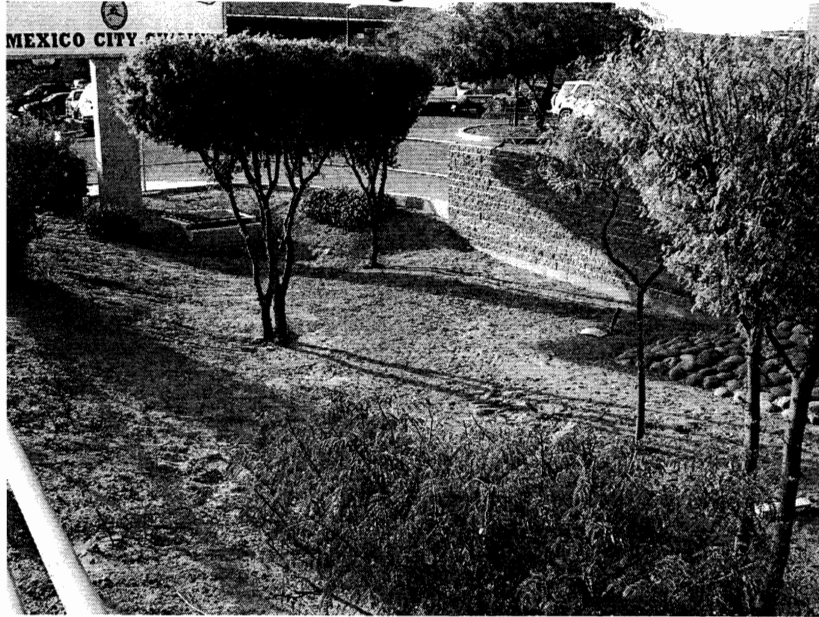
Parking Lot Pond



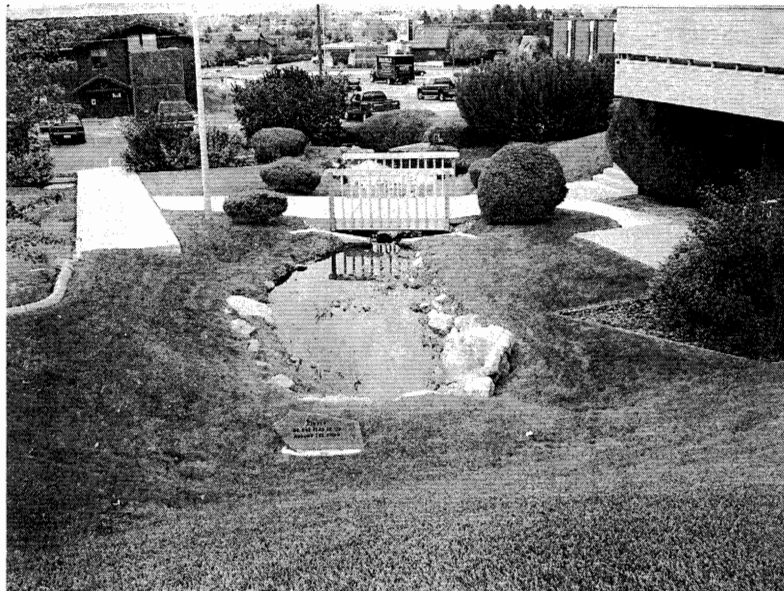
Parking Lot Pond



Parking Lot Pond



Landscaped Pond



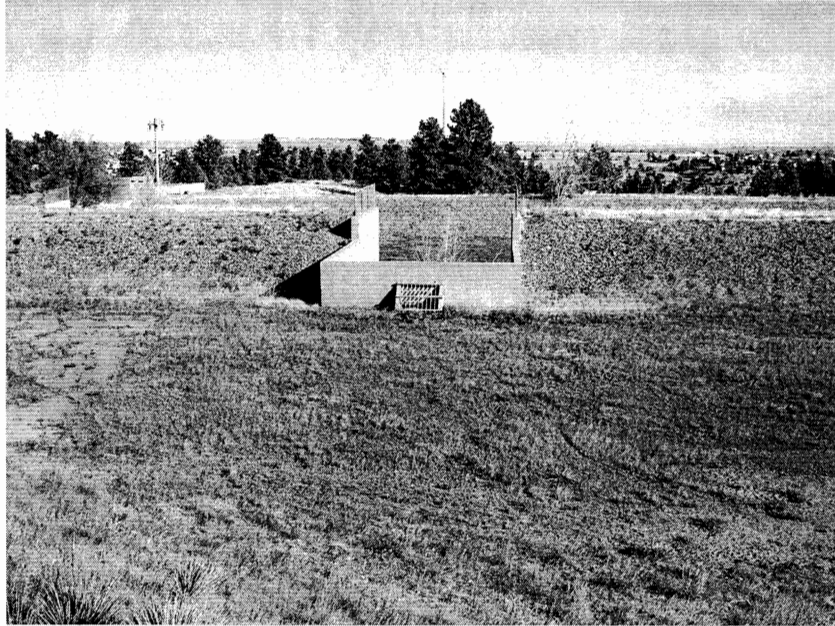
Multiple-function Pond



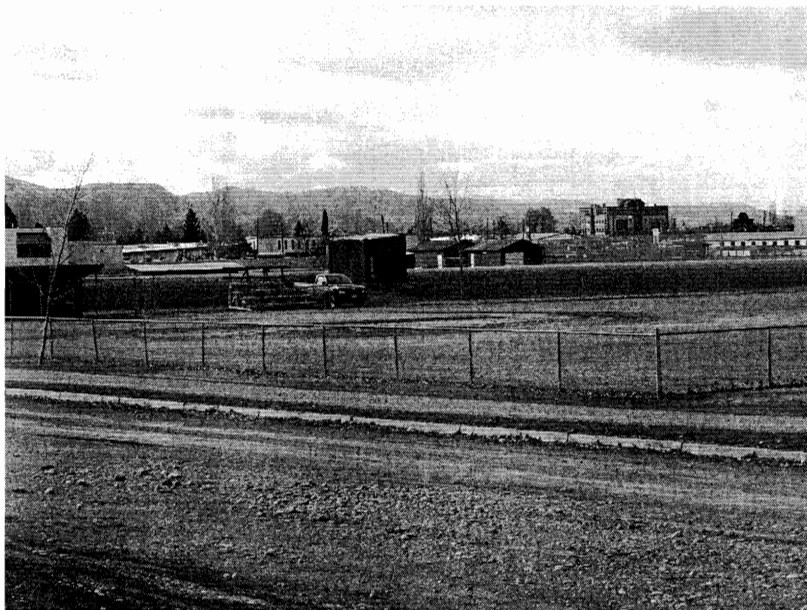
Pond with low-flow channel



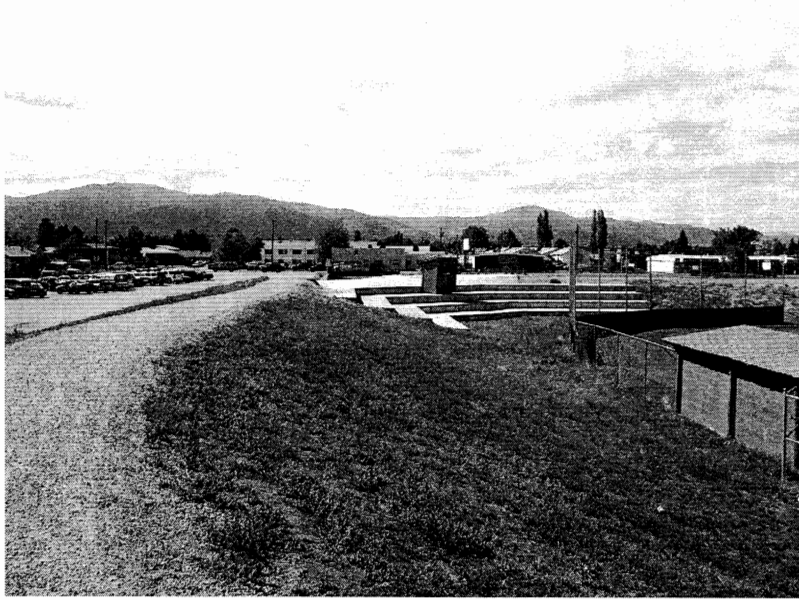
Multiple Ponds in Series



Off-system Pond



Off-system Pond, Outlet



Off-system Pond, Outlet



Off-system Pond, Outlet



Off-system Pond, Outlet



Pond and Inlet



Pond and Inlet - Operating



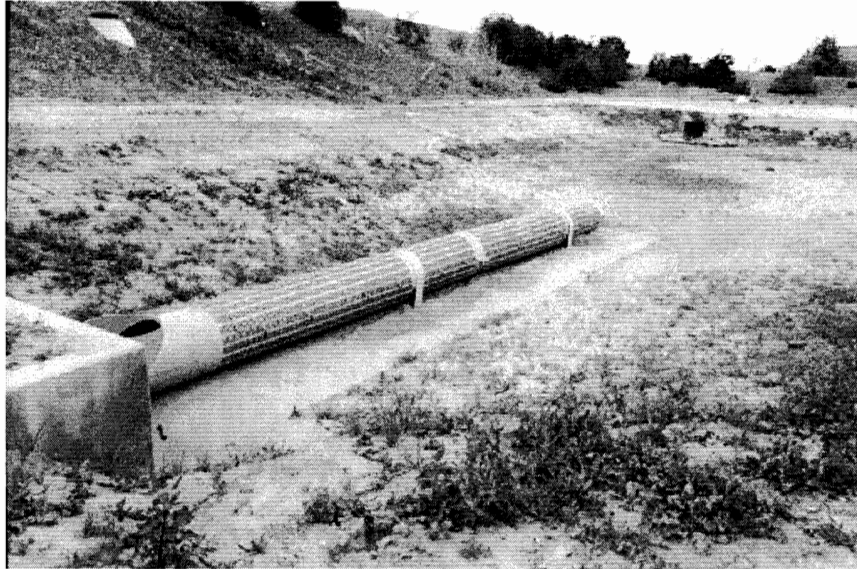
Inlet pipe with trashrack



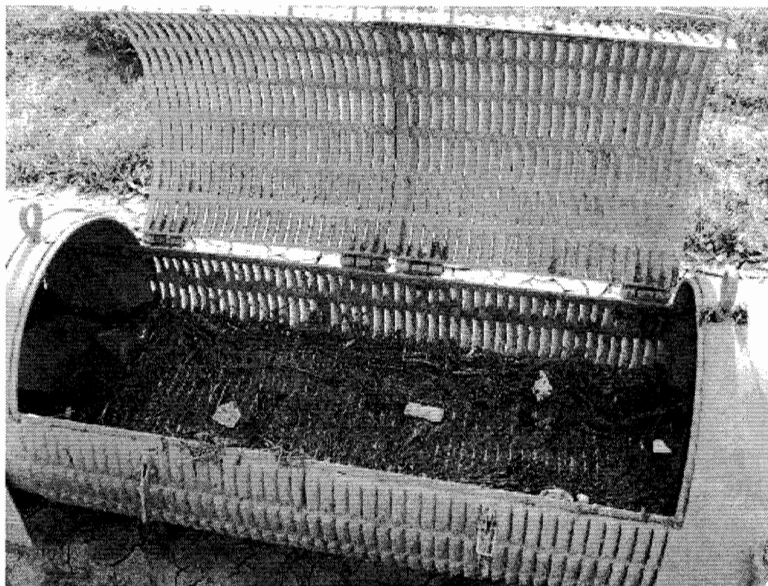
Pond Inlet Structure



Roscoe-Moss Storm Flo™ Screen



Roscoe-Moss Storm Flo™ Screen



Wet Pond



Inlet to Wet Pond

